



U.S. DEPARTMENT OF
ENERGY

Nuclear Energy

Fuel Cycle Research and Development

**Metallic Fuel Casting Development and
Parameter Optimization Simulations**

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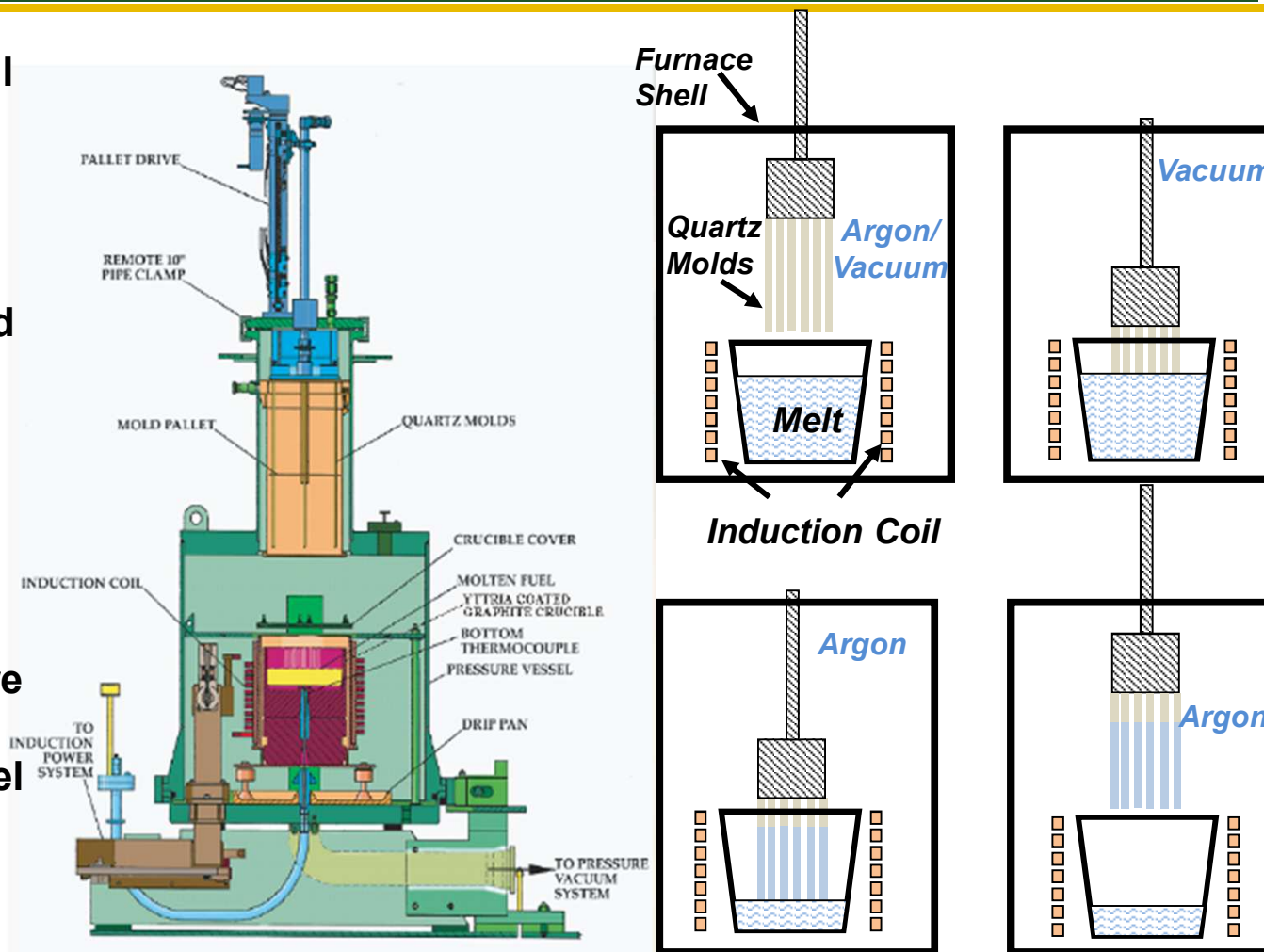
- **Introduction to metallic fuel casting**
 - History
 - Counter-gravity injection casting (CGIC)
- **Current Development Activities**
- **Experimental Results**
- **Parameter Optimization and Simulations**
 - Gas compressibility/venting
 - Surface tension
- **Conclusions**



- **Metallic fuel has been used for several decade in fast reactors**
 - Variety of sized and technologies led to a variety of fabrication methods
 - Fabrication method influence by fuel design and fabrication environment
 - *Large vs. small diameter*
 - *Hands-on/glovebox fabrication vs. remote/hotcell fabrication*
 - Several fabrication methods also used
 - *Deformation processes (extrusion, swaging, etc.)*
 - *Casting*
 - *Combination*
- **EBR-II provided the most recent U.S. experience on larger than laboratory scale**
 - Fuel for the EBR-II was fabricated using the counter gravity injection casting (CGIC) process
 - *Fuel fabrication was done both remotely and hands-on*
 - *Over 130,000 pins were cast and irradiated using this methods*

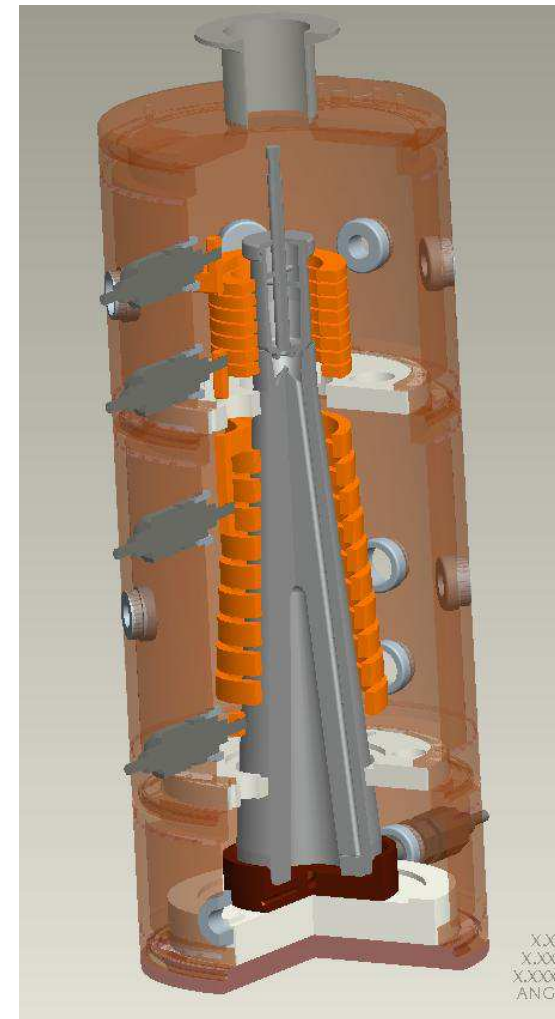


- CGIC worked well but had some efficiency disadvantages
- Large recycle stream- heels and end crops (~40% of melt)
- One time use molds create a large amount of waste
- Reduced pressure may affect transmutation fuel i.e. Am





- **Bottom or gravity pour casting was seen as the lowest risk casting development path**
 - Wide spread industrial use
 - Scale-able from lab to engineering and production use
 - Does not require a reduced pressure (better for Am bearing fuels)
 - Increases melt utilization (large heel is not required and smaller end croppings)
 - Can be used for permanent mold development
- **First system was designed and used for uranium alloys (BCS)**
- **Second system has been designed and is currently being installed for use with Pu and minor actinide bearing casting (GACS)**

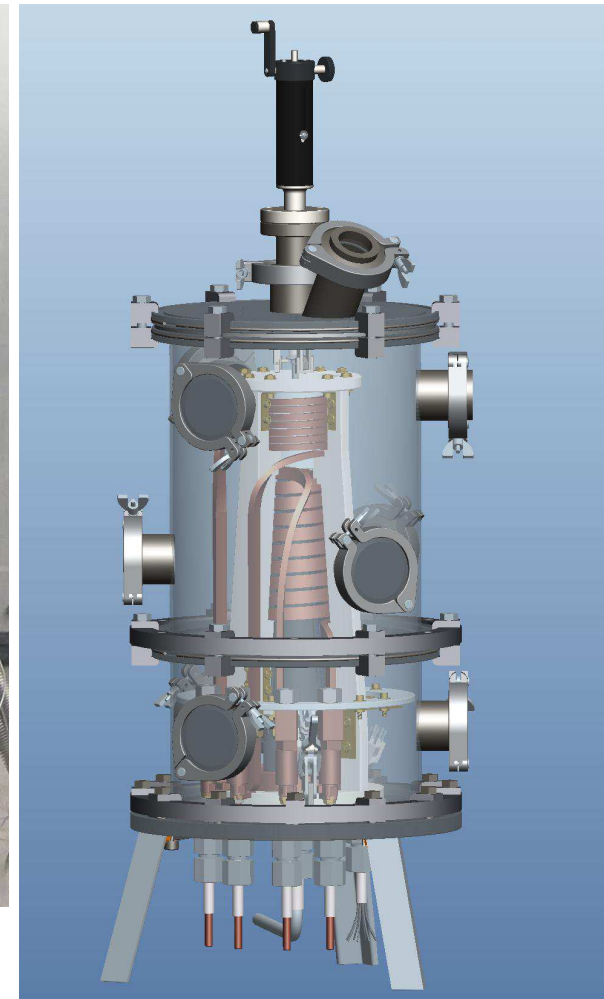




- Initially using Y_2O_3 coated graphite molds and crucibles
- Current fuel slug size: 4.3 mm diameter x 250 mm long
 - Based on EBR-II fuel diameter and was considered to be conservative
- Mold and crucible are independently induction heated
- Designed to allow pressure differential assisted casting i.e. mold can be at a reduced pressure



BCS



GACS

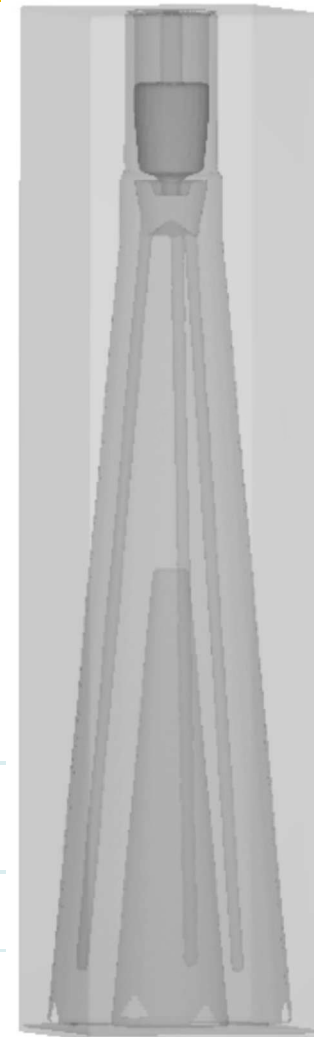


- **A number of parameters were examined with using uranium alloys- amount and time of pressure assist, mold coating vs. no mold coating, mold pre-heating, and super heat amount**
 - Pressure assist caused multiple pin segments
 - No mold coating performed well but resulted in pre-mature freezing (short pins)
 - Level of pre-heating did not have significant effect (800-1000°)
 - Too much super heat lead to pins made of many small segment
 - Mold vent size greatly affects the flow of the material
- **Results high light the need to couple experiments with computations and for better defined molten material properties**





- **Two codes were used for simulations of the casting process**
 - Initially used TRUCHAS when experimental results showed the need for gas compressibility then a switch was made to FLOW-3D
- **Models based on actual BCS/GACS dimensions were developed while casting pressures and temperatures were based on actual casting runs**
- **Basic simulations accounted gravity, heat transfer, and solidification**
 - Surface tension and gas compressibility effects were examined in separate simulations
- **Separate effects testing was done to determine relative importance of thermal and physical properties on casting results**

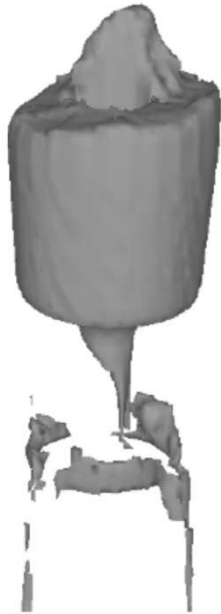


Density	Specific Heat	Thermal Conductivity	Liquidus	Solidus	Latent Heat of Fusion
17.4 g/cm ³	201.3 J/kg· K	26 W/m· K	1340°C	1240°C	38,720 J/kg



Simulations- Venting

- Initial simulation was run assuming the mold was filled with argon at atmospheric pressure with no vents in the mold
- Following simulations placed vents at one of four locations

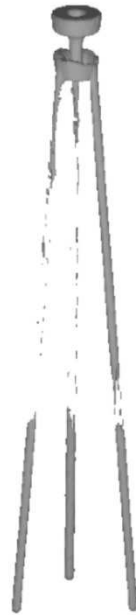


No vent



Bottom

Filling time = 1.7 sec.



Midway

Filling time = 1.7 sec.



Top

Filling time = 2.1 sec.



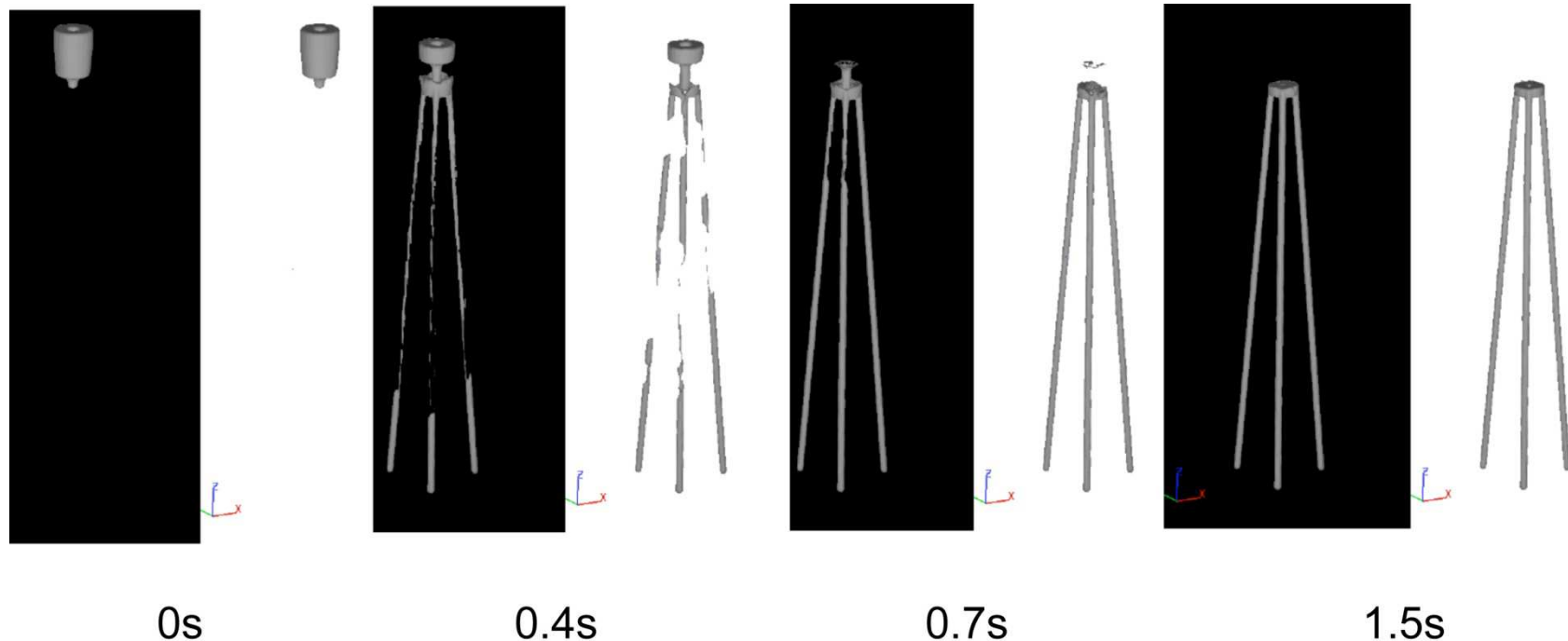
Crucible

Filling time = 1.5 sec.



Simulations- Surface Tension

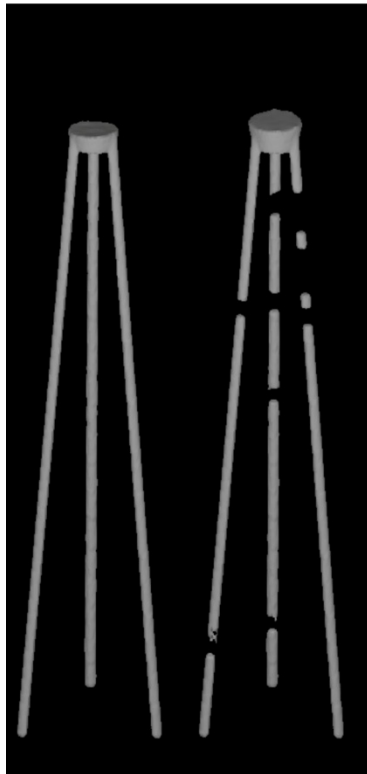
- A value of 1.55 N/m was estimated for U-10Zr
- Simulations were first done using an evacuated mold then a mold initially filled with argon and vented



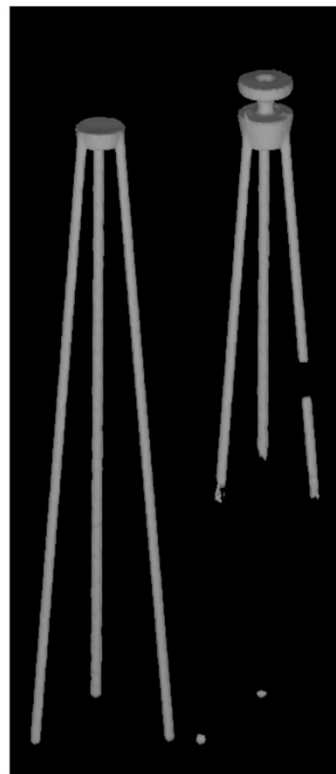
Assumes evacuated mold- left images (black background) does not take surface tension into account



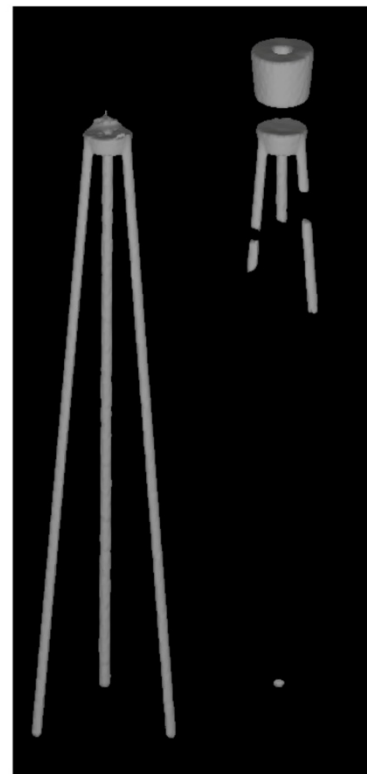
Simulation- Surface Tension



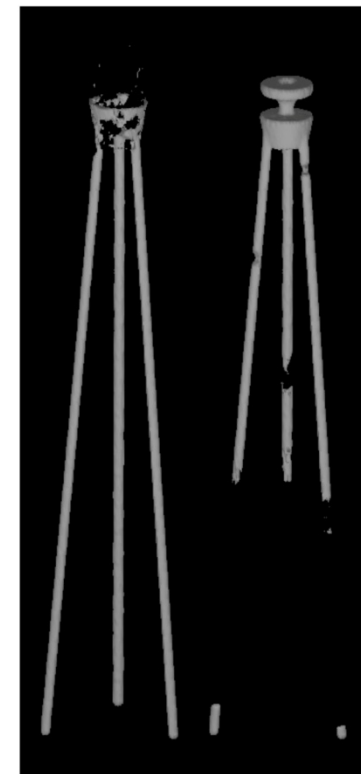
Bottom



Midway



Top



Crucible

Argon filled molds- left images does not take surface tension into account



Simulations- Parameter Optimization

- Several simulations were run to determine the importance of melt/mold wetting angle, surface tension, melt viscosity, and viscosity surface tension relation
- In addition to physical parameters the importance of liquid thermal properties and the effects on casting results was also examined

	Primary	Secondary	Tertiary
Fluid Flow Parameters			
Void Fraction	Wetting angle	Surface tension/viscosity	Surface tension
Solidification	Wetting angle	Surface tension	Surface tension/viscosity
Liquid thermal Properties			
Initial solidification	Heat x-fer coefficient	Latent heat	Specific heat of liquid
Final Solidification	Heat x-fer coefficient	Heat x-fer coefficient	Latent heat

Parameter effect on casting results ranked based on importance



- **Gravity casting is a feasible process for casting of metallic fuels**
 - May not be as robust as CGIC, more parameter dependent to find right “sweet spot” for high quality castings
 - Fluid flow is very important and is affected by mold design, vent size, super heat, etc.
 - Pressure differential assist was found to be detrimental

- **Simulation found that vent location was important to allow adequate filling of mold**
- **Surface tension plays an important role in determining casting quality**
- **Casting and simulations high light the need for better characterized fluid physical and thermal properties**
- **Results from simulations will be incorporated in GACS design such as vent location and physical property characterization**